ZELYAKH, E.V.

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CIRCUITS

"Electric Filters with Resonators of Synthetic Crystals" by Ya. I. Velikin and E. V. Zelyakh, Elektrosvyaz', No 11, November 1957, pp 89-100.

Somewhat obsolete article (delivered at the First All-Union Conference on Piezoelectricity on November 27, 1952, on the development of electric filters for 12-channel carrier telephone system, in which synthetic crystals replace the quartz in the piezoelectric resonators.

Card: 1/1

-3-

SOV/106-58-9-7/17

AUTHOR: Zelyakh, E.V.

The Station-A Crystal Blocking Filter of a 12-Channel TTTLE:

High-Frequency Telephony System (Zagrazhdayushchiy kvartsevyy fil'tr stantsii A 12-kanal'noy sistemy

vysokochastotnogo telefonirovaniya)

PERIODICAL: Elektrosvyaz', 1958, Nr 9, pp 44 - 50 (USSR)

ABSTRACT: The purpose of this filter is to suppress the residual leakage of carriers at 60, 64 108 kc/s which come

through from the modulators of the individual channels. A simplified circuit diagram of the filter is shown in Fig 1. A typical response curve is shown in Fig 2. The

lower scale of this figure shows in more detail the shape of the responses at certain frequencies. In spite of the importance of this filter in a multi-channel system the literature on it is extremely limited. The purpose of

this paper is to provide an analysis and a method of design. Figs 3 and 4 show the familiar equivalent

circuits for a crystal element and equations (7) and (8) Card 1/3 give alternative forms of the expression for the ratio of the two resonant frequencies of the crystal. An

SOV/106-58-9-7/17

The Station-A Crystal Blocking Filter of a 12-Channel High-Frequency Telephony System

important parameter here is the ratio of the "surface" to "internal" capacitances of the crystal. For plates cut at an angle of -18.50 the parameter has a value of 140 and for a +50 cut it has a value of 125. At frequencies sufficiently remote from the carrier frequency, i.e. lying in the pass-bands of the channels, the circuit of Fig 5 is a good representation of the filter action. It will be seen that it is in effect a 2-section m-derived filter. Equation (10) gives the circuit values in terms of cut-off frequency and m. Equation (15) is an expression for the attenuation due to the filter and (16) is its particular value at the cut-off frequency. In the neighbourhood of the carrier frequencies where the attenuation is much greater Fig 6 is a better approximation to the circuit and this may be further reduced to Fig 7. The additional circuit attenuation due to the rapid change in crystal admittance is given by (17), the constituent parts of which are defined in (19) - (22). The attenuation at the carrier

Card 2/3

The Station-A Crystal Blocking Filter of a 12-Channel High-Frequency Telephony System

frequency itself is given by (28). crystal element may be undertaken from (39) for the The design of the inductance, (40) for the resistance, and (41) for the series capacitance. The work was done by A.D. Federov under the guidance of Yani. Velikin. There are 7 figures and 4 references, all Soviet.

ASSOCIATION: Leningradskoye otdeleniye nauchno-issledovatel'skogo instituta svyazi Ministerstva svyazi. (Leningrad Division of the Scientific Research Institute of Communications of the Ministry of Communications,

SUBMITTED: April 21, 1958

Card 3/3

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9.3240 (2301,2901,2902, 2104)

S/109/60/005/012/004/035 E192/E482

AUTHORS:

Zelyakh, E.V. and Lur'ye, B.Ya.

TITLE:

A Method for the Physical Realization of an Ideal

Power Converter

PERIODICAL: Radiotekhnika i elektronika, 1960, Vol.5, No.12,

pp.1895-1901

TEXT: The conception of an ideal power converter as a circuit element was introduced by Zelyakh in 1957 (Ref.1). It is a two-port with matrix

 $\begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} = \begin{bmatrix} \frac{1}{K} & 0 \\ 0 \end{bmatrix} \quad \frac{1}{K}$

Connected in cascade with other two-ports it increases the signal by a factor of K in one direction and by 1/K in the other, independently of the input impedances of the two-ports on either side. Its input impedance is identical with that of the load connected across the output terminals. It was shown (Ref.2) that Card 1/5

S/109/60/005/012/004/035 E192/E482

A Method for the Physical ...

any irreversible two-port can be reduced to a reversible two-port in cascade with an ideal power converter. The physical realization of ideal power converters is the subject of the present article. Analysis shows that the circuit of Fig.l will behave as an ideal power converter under certain conditions. The matrix of Fig.lb is

 $[a] = \begin{bmatrix} \frac{1}{\mu - s} & 0 \\ 0 & \frac{s}{\mu - s} \end{bmatrix}.$

With s=1 this is the matrix of the ideal power converter with $\mu-1=K$. With $s\ne 1$ the circuit is equivalent to the cascade connection of an ideal converter and an ideal transformer. For K to be a real quantity, it is necessary that μ , Z_1 , sZ_1 , Z_2 and Z_3 be real and positive. Stable and real μ over a working bandwidth requires the use of a negative feedback amplifier. If the amplifier is not rigorously unilateral, back-transmission of the signal from the output to the input terminals may be compensated by adjustment of Z_2 and Z_3 . A pentode circuit Card 2/5

S/109/60/005/012/004/035 E192/E482

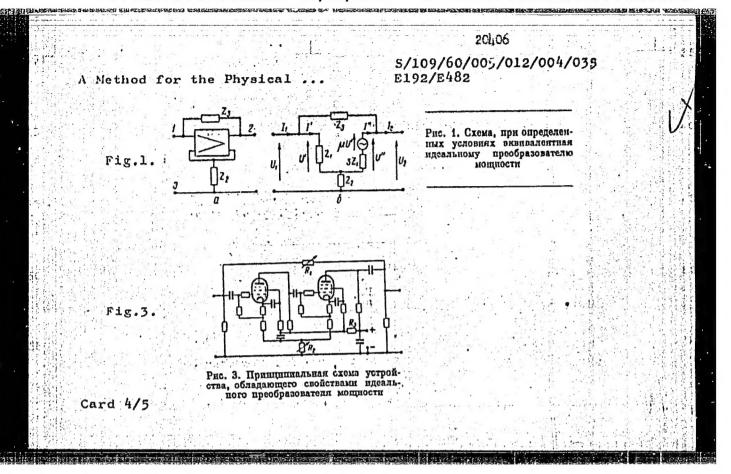
A Method for the Physical ...

modelling Fig.1b is given in Fig.3. The ratio of input to output impedances is very close to unity below 1 MQ. The authors list several applications in measurement techniques. The most interesting application is as a negative-resistance amplifier interesting application is as a negative-resistance amplifier (Fig.4 and 5). Bridging the converter (Fig.4) gives a short-circuit-stable negative-resistance amplifier, putting the impedance in the common lead (Fig.5) gives an open-circuit-stable amplifier. The article closes with stability considerations. There are 5 figures, 1 table and 5 references: 4 Soviet and 1 non-Soviet.

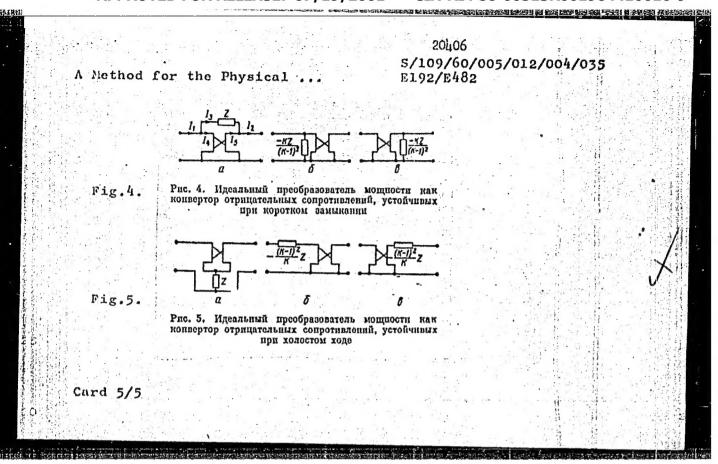
SUBMITTED: May 7, 1960

Card 3/5

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9.3210 (2902, 1031, 1132)

AUTHOR:

Zelyakh, E. V.

TITLE:

On the stability analysis of tube and transistor circuits

PERIODICAL: Elektrosvyaz', no. 7, 1960, 47-59

TEXT: The author describes a method of finding out the characteristic equation of a linear electric circuit, which is required for the circuit stability analysis. The method consists in the representation of the circuit as a quadripole. The purpose of this work is to give a theoretical basis of this method, the foundation for which was laid by the author already in 1929 [Ref. 5: Zelyakh, E. V., "Raschet transformatornykh filtrov" (Calculation of Transformer Filters) (graduation thesis), LETI, 1929]. Theoretically, the method is based on the following five theorems. Theorem I: If a linear electric circuit is reduced to a quadripole with short-circuited poles at both ends, then its characteristic equation has the form

|z| = 0

(1)

where |z| = determinant

Card 1/5

On the stability analysis of ...

$$|z| = \begin{vmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{vmatrix}$$
 (2)

formed from the equation factors of the quadripole

 $\ddot{\textbf{U}}_1$ and $\ddot{\textbf{I}}_1$ represent the voltage and current in the left branch and $\ddot{\textbf{U}}_2$ and $\ddot{\textbf{I}}_2$ in the right branch of the quadripole. Theorem II: If an electric linear circuit is reduced to a quadripole with opened poles, then its characteristic equation has the form

$$|\mathbf{y}| = 0 \tag{6}$$

where
$$|y| = determinant$$

$$\begin{vmatrix} y \\ y \end{vmatrix} = \begin{vmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{vmatrix}$$
(7)

formed from the equation factors of the quadripole

Card 2/5

On the stability analysis of ...

$$\begin{vmatrix}
\dot{1}_1 &= y_{11}\dot{u}_1 + y_{12}\dot{u}_2 \\
\dot{1}_2 &= y_{21}\dot{u}_1 + y_{22}\dot{u}_2
\end{vmatrix} .$$
(8)

Theorem III: If an electric linear circuit is reduced to a quadripole having short-circuited poles at the left branch and open poles at the right branch, then its characteristic equation has the form

$$|\mathbf{d}| = 0 \tag{9}$$

where |d| = determinant

$$\begin{vmatrix} \mathbf{d} \\ \mathbf{d} \end{vmatrix} = \begin{vmatrix} \mathbf{d}_{11} & \mathbf{d}_{12} \\ \mathbf{d}_{21} & \mathbf{d}_{22} \end{vmatrix} \tag{10}$$

formed from the equation factors of the quadripole

$$\dot{\mathbf{U}}_{1} = \mathbf{d}_{11}\dot{\mathbf{U}}_{2} + \mathbf{d}_{12}\dot{\mathbf{I}}_{1}
\dot{\mathbf{I}}_{2} = \mathbf{d}_{21}\dot{\mathbf{U}}_{2} + \mathbf{d}_{22}\dot{\mathbf{I}}_{1}$$
(11)

Theorem IV: If an electric linear circuit is reduced to a quadripole having short-circuited poles at the right branch and opened poles at the left branch, then its characteristic equation has the form

Card 3/5

21199 s/106/60/000/007/002/003/xx On the stability analysis of... |f| = 0 (14) where f = determinant $|f| = \begin{vmatrix} f_{11} & f_{12} \\ f_{21} & f_{22} \end{vmatrix}$ (15) formed from the equation factors of the quadripole

$$\dot{\hat{I}}_{2} = f_{11}\dot{\hat{I}}_{1} + f_{12}\dot{\hat{I}}_{2}
\dot{\hat{I}}_{1} = f_{12}\dot{\hat{I}}_{1} + f_{22}\dot{\hat{I}}_{2}$$
(16)

Theorem V: If an electric linear circuit is reduced to a ring circuit, then its characteristic equation has the form

$$a_{11} + a_{22} = |a| + 1 \tag{17}$$

where
$$|a| = determinant$$
 $\begin{vmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{vmatrix}$ (18)

formed from the equation factors of the quadripole

Card 4/5

On the stability analysis of ...

(19)

Proofs for the above mentioned theorems are given. Tables list the characteristic equations of the quadripoles for the different connections of its poles, the characteristic equations for some circuits containing an ideal tube or semiconductor period and characteristic equations for some ring circuits containing a tube, or a transistor, connected to a reversible quadripole. Examples of practical application of this method are given. Appendix 1 gives matrices of an electron tube connected as a quadripole. Appendix 2 gives matrices for a transistor in an equivalent T-circuit with viet-bloc and 2 non-Soviet-bloc. The references to the English-language publications read as follows: 1) Oakes, "Analysis of junction transistor audio oscillator circuits", Proc. IRE, vol. 42, no. 8, 1954. 2) Honnell, The generalized transmission matrix stability criterion", Trans. AIEE, vol. 1951.

SUBMITTED: March 10, 1960.

Card 5/5

s/106/60/000/011/004/010 A055/A033

9,7550

AUTHORS:

Card 1/2

Velikin, Ya.I., Gel'mont, Z.Ya., and Zelyakh, E.V.

TITLE:

A Piezoelectric Band-Elimination Filter Circuit.

PERIODICAL: Elektrosvyaz', 1960, No.11, pp. 34-39

TEXT: The band-elimination quartz filters have usually a comparatively low impedance in the region of the suppressed frequencies. In some practical cases, it is sometimes necessary, however, for the filter to have a considerable impedance in the suppressed band. Two such filter circuits, a containing one and two piezoelectric resonators respectively (see Fig. 1a and 1b) are described in the present article. These filter circuits have really two suppression bands: a wide one and a narrow one. The narrow band, in the region of the antiresonance frequency of the resonator (shunted by a capacitance), is the principal one and is used for the suppression of currents of given frequencies. Its width is somewhat larger in the circuit containing two resonators. Using equivalent circuits for his discussion, the author calculates the effective attenuation in the suppression band. He establishes first a general formula for the case of the filter circuit con-

S/106/60/000/011/004/010 A055/A033

A Piezoelectric Band-Elimination Filter Circuit.

taining two resonators, and then applies this formula to the filter circuit with one resonator. He then works out a corresponding formula for the effective attenuation in the transmission band of the filters. Formulae are also given allowing to calculate the input impedance of the filter circuit case of the pass-band (simplified approximate formulae being used in the latter case). At the end of the article, some general recommendations are given as to the calculation of the filter circuits and the choice of the piezoelectric resonators. There are 7 figures and 6 references: 5 Soviet and 1 non-Soviet.

SUBMITTED: May 3, 1960

Puc. 1 0 b)

Card 2/2

s/108/60/015/008/002/006 B012/B067

9.3240

AUTHOR:

Zelyakh, E. V., Member of the Society

TITLE:

A New Theory of the Autonomous Four-pole and Its Application to an Amplifier With Distributed Amplification

Radiotekhnika, 1960, Vol. 15, No. 8, pp. 13-24

PERIODICAL:

TEXT: The fundamentals of the present paper were outlined on April 26, 1954, at the Scientific-technical Conference of the Leningradskiy elektrotekhnicheskiy institut svyazi im. M. A. Bonch-Bruyevicha (Leningrad Electrotechnical Institute of Communications imeni M. Bonch-Bruyevich) and on May 13, 1958, at the All-Union Scientific Session of the NTORIE im. A. S. Popova (NTORIE imeni A. S. Popov) held in Moscow on the occasion of the Day of Radio. In his earlier papers (Refs. 1,2) the author developed the theory of an autonomous four-pole. A four-pole containing independent energy sources is termed an autonomous four-pole. Such a four-pole independently produces (autonomous) voltages and currents at its external terminals. The theory is based on the use of no-load

Card 1/3

A New Theory of the Autonomous Four-pole and Its Application to an Amplifier With Distributed Amplification 82865 s/108/60/015/008/002/006 B012/B067

voltages and short-circuit currents (measured at the terminals of the four-pole switched off from the current circuit) as autonomous parameters. Together with the coefficients of the four-pole equations these parameters allow the calculation of various regular four-pole systems if there are no restrictions concerning the selection of these systems. In practice, however, certain restrictions are imposed for simplifying the calculation in various systems. In the paper (Ref. 3) such a calculation was made for nonautonomous four-poles. Here, a similar system of parameters is given for autonomous four-poles. Only autonomous circuits whose "body" is a symmetrical four-pole are dealt with. The "body" of an autonomous four-pole is the nonautonomous four-pole which is obtained from the corresponding autonomous four-pole if in the latter the control voltages and the control currents of all independent sources are assumed to vanish. New parameters are introduced for the autonomous four-pole which are termed characteristic voltages and currents. The author established the relation between the latter and the other autonomous parameters. In the following, the theory of a cascade circuit

Card 2/3

A New Theory of the Autonomous Four-pole and Its Application to an Amplifier With Distributed Amplification

82865 \$/108/60/015/008/002/006 B012/B067

of accordant autonomous four-poles with symmetrical bodies is set up. Formulas for calculating the voltages and currents at the current circuit terminals are derived for any loads. Tables 1-5 show formulas for the characteristic voltages and currents of some typical four-poles. To illustrate the theory explained it is applied to analyzing an amplifier with distributed amplification (Fig. 14). Formulas for the amplification coefficient of the amplifier are derived taking account of the mismatch at both ends of the grid- and anode current circuit. It is shown that the analysis made on the basis of the theory of autonomous characteristic parameters is simpler and more illustrative than the analysis of the amplifier of papers (Refs. 5,6), and that more general results are obtained. It is pointed out that the theory presented here may also be used for analyzing receiving antennas, lines with noises, etc. There are 16 figures, 5 tables, and 8 references: 6 Soviet and 2 US.

SUBMITTED:

June 12, 1959

Card 3/3

30136 S/194/61/000/007/061/079 D201/D305

9.3230 (1132,1159)

AUTHOR:

Zelyakh, E.V.

TITLE:

Signs of the characteristic parameters of symmetrical four-poles containing negative resistances

PERIODICAL:

Referativnyy zhurnal. Avtomatika i radioelektronika, no. 7, 1961, 9, abstract 7 172 (V sb. 100 let so dnya rozhd. A.S. Popova, M., AN SSSR, 1960, 160-170)

TEXT: The characteristic parameters of symmetrical fourpoles (F) (the characteristic impedance $\mathbf{Z_C}$ and the char. transmission constant $\mathbf{g_C}$) are expressed by radicals, whose choice of signs is of importance both in theory and practice. The present work is an endeavor to make this problem completely clear. By considering the known F equations

 $\dot{v}_1 = \text{ch } g_c \ v_2 + Z_c \text{ sh } g_c \ \dot{i}_2$ $\dot{i}_1 = \frac{1}{Z_c} \text{ sh } g_c \ \dot{v}_2 + \text{ch } g_c \ \dot{i}_2$

Card 1/2

X

30136 S/194/61/000/007/061/079 D201/D305

Signs of the characteristic ...

it is shown that the sign of one of the characteristic parameters is closely related to that of the other. The latter of the signs may be determined either analytically or graphically. In the analytical determination of signs of the charact. parameters, formulae are used which relate to each other $\mathbf{Z}_{\mathbf{C}}$ and $\mathbf{g}_{\mathbf{C}}$ and any other single valued parameters of $\mathbf{F}_{\mathbf{I}}$ e.g.

 $\frac{z_c}{\text{th } g_c} = Z_{x.x}; Z_c \text{ th } g_c = Z_{k.3}$

The graphical sign determination is based on topological properties of the rand Z_k z as formulated by Feldtkeller. Several theorems based on the theory introduced above, are given. These theorems make it possible to determine directly for many F the signs of charact. parameters. Examples of application of the theory are given. 5 references. Abstracter's note: Complete translation

Card 2/2

9.2186 (1063,1159) 9.3230 (1132,1040) 2587 S/108/61/016/011/003/007 D201/D304

AUTHORS:

Velikin, Ya.I., Gel'mont, Z.Ya., and Zelakh E.V.,

Members of the Society

TITLE:

Narrow-band lattice crystal filters

PERIODICAL: Radiotekhnika, v. , no. 11, 1961, 26 - 33

TEXT: In the present article design formulae are derived for lattice filters consisting of a piezoelectric crystal and a capacitor and forming a single, two-, three and four-section networks. The analysis of the filters is made using basic it and T-sections, as shown in Figs. la and 2a. Although design formulae for the above configuration are given in literature, for narrow pass-band filters, in which the ratio of the pass-band to its center frequency is smaller than e.g. 0.05, simpler approximate formulae may be used obtained by the method similar to that given by V. Zelakh (Ref. 6: Metod rascheta ekvivalentnykh skhem (Method of Designing Equivalent Circuits Nauchno-tekhn. sb. po elektrosvyazi Leningr. in-ta svyazi no. 6, 1946). These formulae are as follows: for N-section Card 1/6

29587 S/108/61/016/011/003/007 D201/D304

Narrow-band lattice crystal filters

$$c_1 \approx \frac{1 - m^2}{4\pi m f_a R_{nom}} \tag{1}$$

$$\sigma_2 \approx \frac{m}{2\pi f_a R_{nom}}$$
 (2)

$$c_q \approx \frac{\Delta}{2\pi \text{ mf}_a^2 \text{ R}_{nom}}$$

L_q
$$\approx \frac{mR_{nom}}{2\pi\Delta}$$
;

for T-section

$$c_1 \approx \frac{m}{2\pi f_a R_{nom}}$$

$$c_2 \approx \frac{2}{3(m^2-1)} f_a R_{nom}$$

$$c_{q} \approx \frac{2m^{3} \Delta}{\pi (m^{2}-1)^{2} f_{a} R_{nom}}, \quad L_{q} \approx \frac{(m^{2}-1)^{2} R_{nom}}{8\pi m^{3} \Delta}.$$

$$L_{q} \approx \frac{(m^2 - 1)^2 R_{nom}}{8 \pi m^3 \Delta}.$$

Card 2/6

29587 S/108/61/016/011/003/007 Narrow-band lattice crystal filters D201/D304

For both cases $\sqrt{\frac{f_2^2 - f_2^2}{2}}$

$$\mathbf{m} = \sqrt{\frac{12}{\mathbf{f}_1^2 - \mathbf{f}_{\infty}^2}} \tag{3}$$

and $\Delta = f_2 - f_1, f_a = \frac{1}{2} (f_1 + f_2)$ (4)

where f_1 and f_2 out-off frequencies, f_{00} - frequences of the attenuation band, R_{nom} - characteristic filter impedance at frequency f_{a^0} For narrow-band filters, as frequencies near f_a

$$m \approx \sqrt{\frac{f_2 - f_{\infty}}{f_1 - f_{\infty}}} \tag{5}$$

may be assumed and hince, introducing

$$\Delta_{\infty} = 2(f_{\infty} - f_{a}), \quad t = \frac{\Delta_{\infty}}{\Delta}$$
 (6)

Card 3/6

Narrow-band lattice crystal filters

29587 S/108/61/016/011/003/007 D201/D304

the approximate expression for m is obtained as

$$\mathbf{m} \approx \sqrt{\frac{5-1}{t+1}} \,, \tag{7}$$

which is the generalized equation (does not contain frequency). The attenuation of the single section filter is derived as

$$N \approx \frac{1}{2} \sqrt{t^2 - 1} \frac{\frac{1}{\alpha} - \alpha + (\frac{1}{\alpha} + \alpha)\eta}{\eta - t}$$
 (22)

where $\alpha = \frac{R_0}{R_{nom}}$, and η given by

$$\eta = \frac{f - f_{A}}{\frac{1}{2}\Delta} \tag{19}$$

- the normalized frequency (Ref. 6: Op. cit.). For the two-section filter the anntenuation is derived as

Card 4,/6

²⁹⁵⁸⁷ \$/108/61/016/011/003/007

Narrow-band lattice crystal filters

$$N \approx \sqrt{t^2 - 1} \frac{\left[\frac{1}{\alpha} - \alpha + \left(\frac{1}{\alpha} + \alpha\right)\eta\right](\eta t - 1)}{(\eta - t)^2}, \tag{27}$$

for three-section

for three-section
$$N \approx \frac{1}{2} \sqrt{t^2 - 1 \left[\frac{1}{\alpha} - \alpha + (\frac{1}{\alpha} + \alpha)\eta\right]} \frac{4(\eta t - 1)^2 - (t - \eta)^2}{(t - \eta)^3}$$
(35)

and four-section as

and four-section as
$$N = 2\sqrt{t^2 - 1} \left[\frac{1}{\alpha} - \alpha + (\alpha + \frac{1}{\alpha}) \eta \right] (\eta t - 1) \frac{2(\eta t - 1)^2 - (\eta - t)^2}{(\eta - t)^4};$$

Each of tehm simplifies according to the values of load and the respectiv values of η and t. The above filter circuits may, in particular be used for crystal filters at frequencies above 1 mc/s, with transverse oscillating crystals of AT and BT cut. Experimental two—and three—Π—section filters operating at the center pass—band frequency of 1364 kc/s had a pass band of 8CO c/s. There are 8 figures and 7 references: 4 Soviet—bloc and 3 non—Soviet—bloc. The Card 5/6

Narrow-band lattice crystal filters

29587 S/108/61/016/011/003/007

Preference to the English-language publication reads as follows: R.

A. Sykes, IRE National Convention; part 2, 1958.

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosyyazi im. A.S. Popova (Scientific and Technical Communication im. A.S. Popova (Scientific and Technical Communication taken from 1st page of journal)

SUBMITTED: April 29, 1960 (initially)

July 7, 1961 (after revision)

Fig. 1.

Gard 6/6

S/106/62/000/002/008/010 A055/A101

9,2186 authors:

Velikin, Ya. I., Zelyakh, E. V., Ivanova, A. I.

TITLE:

Single-mesh narrow-band magnetostrictive filters

PERIODICAL: Elektrosvyaz', no. 2, 1962, 51 - 59

TEXT: In the present article are described some of the results of the study of magnetostrictive ferrite-core resonators and of filters composed of such resonators, undertaken by the authors. Only single-mesh narrow-band filters are examined in this article, by the analytical method already described by two of the authors (Zelyakh and Velikin, Radiotekhnika, no. 7 - 8, 1946). The sche-of the authors (Zelyakh and Velikin, Radiotekhnika, no. 7 - 8, 1946). The sche-of the authors (Iters is shown in Fig. 1a, Fig. 1b being its equivalent matic diagram of these filters is shown in Fig. 1a, Fig. 1b being its equivalent circuit. Neglecting, as a first approximation, the losses in the filter elements, the authors derive expressions permitting the calculation of the filter elements L_{01} , L_{02} , L_{1} , L_{2} , C_{1} and C_{2} (or the elements L_{0} , L_{1} , C_{1} and C_{2} when elements L_{01} , L_{02} , L_{1} , L_{2} , C_{1} and C_{2} (or the elements L_{0} , L_{1} , L_{2} , C_{1} and C_{2} when $L_{1} = L_{2} = L$ and $L_{01} = L_{02} = L_{0}$). They next calculate the components of the magnetostrictive resonator impedance Z = R + iX. Formulae are deduced, first for netostrictive resonator impedance Z = R + iX. Formulae are deduced, first for resonators forming the first and the second arm of the filter, respectively. Expressionators forming the first and the second arm of the filter, respectively.

Card 1/2

Single-mesh narrow-band magnetostrictive filters

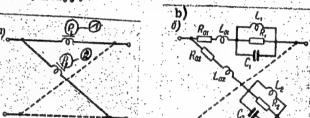
S/106/62/000/002/008/010 A055/A101

perimental checks proved that the values of the resistances and reactances calculated with the aid of these formulae are sufficiently correct. In the third chapter of the article, the authors determine the working attenuation of the examined filters in two cases: 1) without taking into account the losses in the resonators, 2) account taken of these losses. The results of an experimental investigation of some magnetostrictive filters designed according to the described method are reproduced at the end of the article. There are 10 figures and 5 references: 4 Soviet-bloc and 1 non-Soviet-bloc. The reference to the English-language publication reads as follows: Burgt. Piezomagnetic ferrites. Electronic Technology, 1960, v. 37, no. 9. The Soviet authors or scientists mentioned in the article are: S. S. Kogan, N. D. Bosyy.

SUEMITTED: June 23, 1961

Figure 1. Legend 1 - Res₁ 2 - Res₂

Card 2/2



5/106/62/000/004/007/010 A055/A101

9,2186

AUTHORS:

Velikin, Ya.I.; Zelyakh, E.V.; Ivanova, A.I.

TITLE:

Rejection magnetostrictive filters

PERIODICAL: Elektrosvyaz', no. 4, 1962, 48 - 54

A method for calculating bridge-type rejection filters consisting of magnetostrictive resonators and condensers is described. The rejection magnetostrictive filter is shown schematically in Figure 1, the resonator being replaced by its equivalent circuit (the losses in the filter elements are neglected). impedances of the arms are:

 $Z_1 = 12\pi f L_0 \frac{f_2^2 - f^2}{f_2^2 - f^2}; \quad Z_2 = \frac{1}{12\pi f C_2},$ (1)

where f1 and f2 are, respectively, the antiresonant and the resonant frequency of the resonator. The filter characteristic impedances Z_{CO} and $Z_{C\infty}$ (at f = 0 and $f \to \infty$, respectively) being but little different, the rated impedance of the filter is taken equal to

S/106/62/000/004/007/010 A055/A101'

Rejection magnetostrictive filters

$$Z_{m} = \sqrt{\frac{L_{0}}{c_{2}}} = \frac{R_{0}}{\alpha} , \qquad (3)$$

 R_0 being the load resistance and ∞ the matching coefficient. The graphs showing the frequency-dependence of Z_1 , Z_2 , b_c (characteristic attenuation) and Z_c reveal that the examined circuit is a rejection filter whose characteristic rejection band is situated between the frequencies f_1 and f_2 . Within this band (at f_{∞}), occurs the attenuation pole, f_{∞} being deduced from formula: $f_{\infty}^{2}(f_{2}^{2}-f_{\infty}^{2})=F_{0}^{2}(f_{\infty}^{2}-f_{1}^{2}),$

$$f_{\infty}^{2}(f_{2}^{2}-f_{\infty}^{2})=F_{0}^{2}(f_{\infty}^{2}-f_{1}^{2})$$
, (4)

where

$$F_0 = \frac{1}{2\pi\sqrt{L_0 c_2}} \tag{5}$$

The formulae permitting the calculation of the filter elements are:

$$L_0 = \frac{Z_m}{2\pi F_0}$$
, $L_1 \approx L_0 \frac{2\Delta}{f_1}$, $C_1 = \frac{1}{4\pi^2 f_1^2 L_1}$, $C_2 = \frac{1}{2\pi F_0 Z_m}$, (6)

Card 2/4

Rejection magnetostrictive filters

S/106/62/000/004/007/010 A055/A101

$$F_0 = f_{\infty} \sqrt{\frac{f_2^2 - f_{\infty}^2}{f_{\infty}^2 - f_1^2}} \approx f_{\infty} \sqrt{\frac{f_2 - f_{\infty}}{f_{\infty} - f_1}}$$
 (7)

 Δ = f_2 - f_1 being the width of the characteristic rejection band. The maximum width of the rejection band is:

$$\Delta_{\max} = \frac{1}{2} K^2 f_1 \tag{8}$$

K being the electromechanical coupling coefficient. The author next considers the case when two rejection bands are necessary (two series-connected magneto-strictive resonators being used) and deduces a formula giving $\Delta_{\rm max}$ for this case. He calculates then the working attenuation of the single-mesh filter. This attenuation is:

$$b_{\text{work}} = \ln \sqrt{1 + \frac{1 - t^2}{4} \frac{\left[(\alpha - \frac{1}{\alpha}) \eta + \alpha + \frac{1}{\alpha} \right]^2}{(\eta - t)^2}},$$
 (16)

where
$$t = \frac{\Delta_{\infty}}{\Delta}$$
, $\Delta_{\infty} = 2 (f_{\infty} - f_a)$, $f_a = \frac{1}{2} (f_1 + f_2)$, $\eta = \frac{2 (f - f_a)}{\Delta}$. An

S/106/62/000/004/007/010 A055/A101

Rejection magnetostrictive filters

analogous formula is also deduced for the working attenuation of the two-mesh filter. Some results of a practical application of the above formulae are given at the end of the article. The Soviet personalities mentioned in the article are: D.G. Yatsenko, T.M. Novikova, N.D. Bosyy. There are 9 figures and 4 references: 3 Soviet-bloc and 1 non-Soviet-bloc.

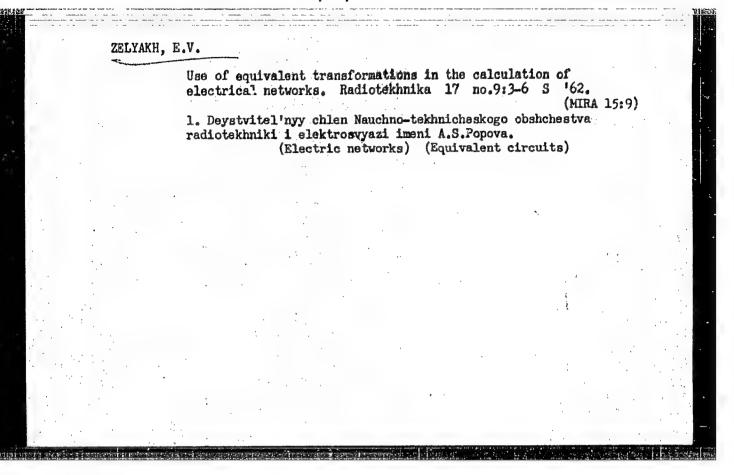
SUBMITTED: October 28, 1961

Figure 1b.

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"APPROVED FOR RELEASE: 07/19/2001 CIA-RDP86-00513R001964410016-9

VELIKIN, Ya.I.; ZELYAKH, E.V.; IVANOVA, A.I.

Wide-band magnetostrictive filters. Elektrosviaz' 17 no.10:1-9 0
(MIRA 17:1)

163.

Canonical schematics of two-terminal circuits consisting of two-terminal networks of two forms. Radiotekhnika 20 no.7:1-8 Jl *65.

1. Deystvitel nye chleny Nauchno-tekhnicheskogo obshchestva radiotekhniki i elektrosvyazi imeni Popova.

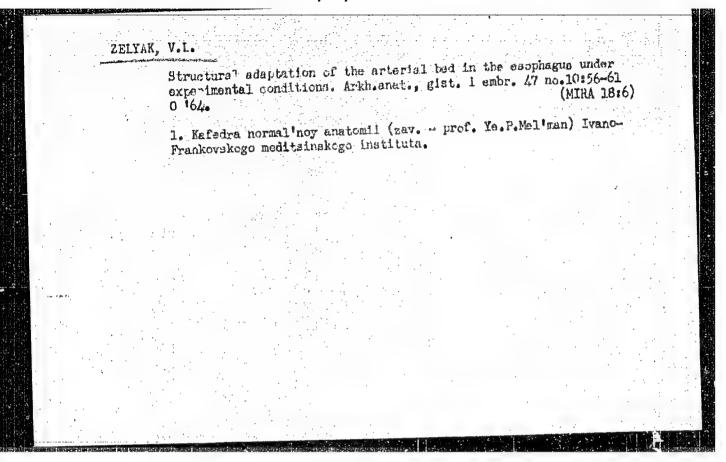
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Card 1/2

CIA-RDP86-00513R001964410016-9

SOURCE CODE: UR/0106/66/000/002/0001/0008 EWT(1) L 35854-66 ACC NR: AP6010785 AUTHOR: Velikin, Ya. I.; Zelyakh, E. V.; Ivanova, A. I. ORG: none TITLE: Narrow-band magnetostriction filters 15 SOURCE: Elektrosvyaz', no. 2, 1966, 1-8 TOPIC TAGS: electric filter, magnetostriction filter ABSTRACT: A method is developed for calculating single- and two-section magnetobridge circuit and include one twowinding magnetostriction resonator and one doubly-wound inductance coil (see figure). Theoretical plots of characteristic impedance and attenuation of MF arms are shown. Formulas for the effective attenuation of single- and two-section MF's Equivalent Actual Magnetostriction-filter circuit UDC: 621, 372, 542, 22

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Evaluating the masses of globular clusters. Uch.zap.LGU no.190:52-58 '57. (MLRA 10:7)

ZELYAK, V.L.

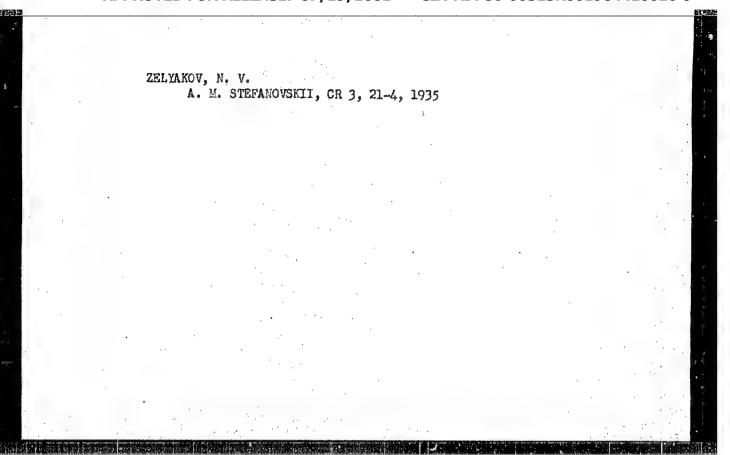
Distribution and plasticity of intraorganic arteries in the esophagus of dogs. Dop. AN URSR no. 6:814-817 '64.

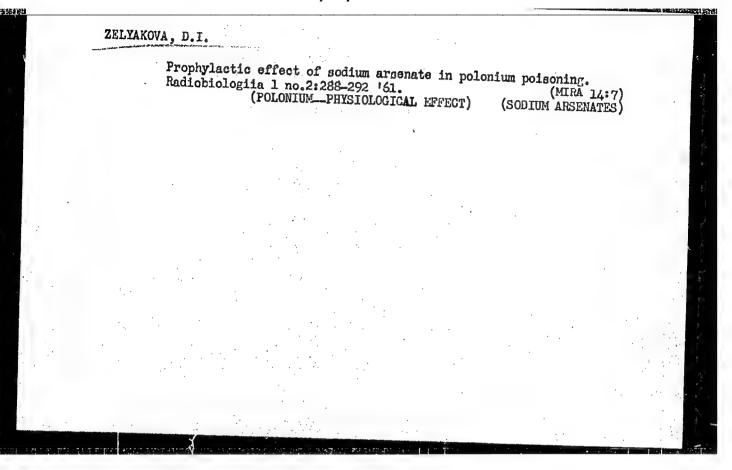
(MIRA 17:9)

1. Ivano-Frankovskiy gosudarstvennyy meditsinskiy institut. Predstavleno akademikom AN UkrSSR V.G.Kas'yanenko [Kas'ianenko, V.H.].

ZELYaKOVA, D. I., Cand Med Sci — (diss) "Reaction of an organ affected with relenium to the action of arsenic," Moscow, 1960, 13 pp (Academy of Medical Sciences USER)

(KL, 38-60, 110)





ZELYAKOVA, D.I. (Moskva)

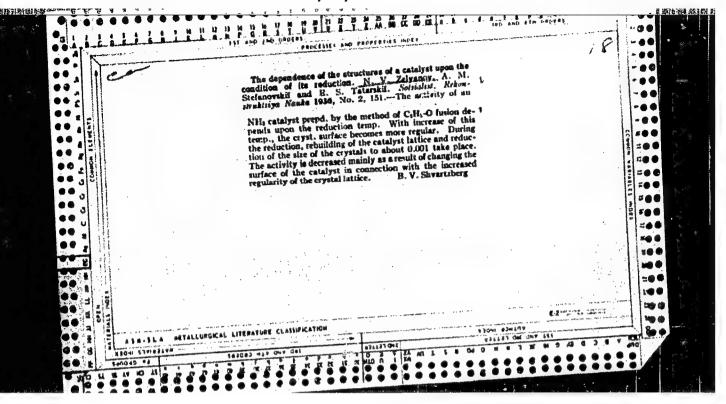
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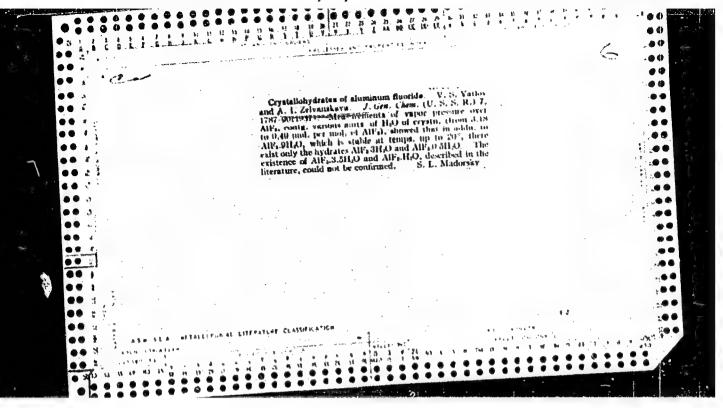
1. Submitted September 5, 1963.

ZELYANKEVICH, V.M.

Their school is their home. Rab.i sial. 37 no.11:14-15 H '61. (HIRA 14:10)

1. Direktor Pruzhanskoy shkoly-internata.
(Fruzhany District - Boarding schools)





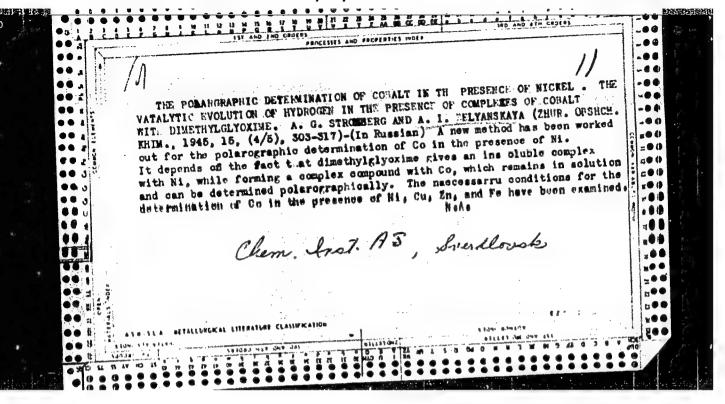
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"Viscosity of Solutions of Alkali Chromates." Zhur. Prikl. Khim., 12, 1939.

ZELYANSKAYA, A. I., RYSS, I. G., and ZAYARNYY, A. E.

"Preparation of Crystallized Chromic Anhydride from Calcium Chromate." Zhur. Prim. Khim., 14, 46-61, 1941.

A boiling mixt. of 456 g./l. Na CrO, 29.6 g./l. Na SO and traces of free alkali was treated with an equiv. quantity of a soln. contg. CaCl 33. KCl 2.64, and KClO 0.75%. The filtered and washed CaCrO was decompd. with H SO and the soln. of CrO obtained was filtered and concd. to about 66%. Yield of CrO was 97%-98%. The corrosium resistance of materials to be used as evaporators, reactors, etc., was found to be (loss in g./sq. m./hr. on exposire to process conditions for 0-2 and 2-4 hrs.. resp.): Gray cast iron (C 3.39. Si 2.94, Mn 0.55, P 0.217 and S 0.06%) 6.58 and 2.65; boiler blate of the Chusovo mills (C 0.172, Mn 0.34, P 0.032, S 0.042% and Sitraces) 1.77 and 3.23; iron of the Armeo type (C 0.025, Mn 0.035, S 0.025 and P 0.009%) 32.6 and 15.84; sheet aluminum 103.0 and 2.42. Rolled lead (Bi 0.004, Cu 0.005, Fe 0.003 and Sb 0.011%) in 3 hrs lost 259.6



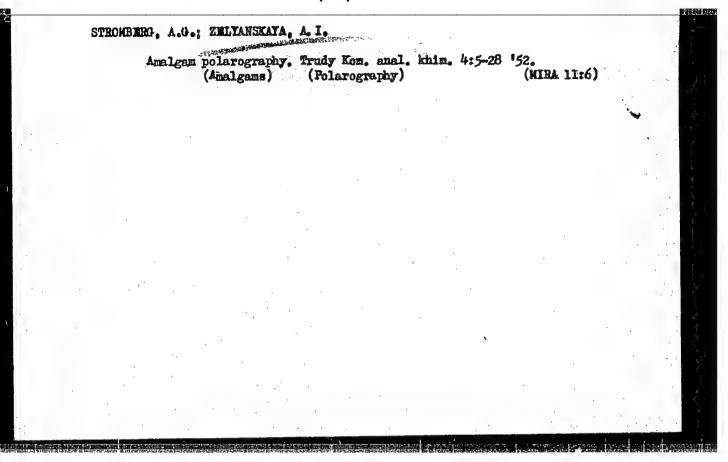
ZFLYANSKAYA, A. I.

Mbr., Inst. Chemistry & Metallurgy; Ural Affil., Acad. Sci., -1944-c49-.

"Polarographic Determination of Cobalt in the Presence of Nickel. Catalytic Evolution of Hydrogen in the Presence of Complex Compounds of Cobalt with Direthyl-glioxyr," Zhur. Obshch. Khim., 15, Nos. 4-5, 1945;

"Study of the Solubility of Dimethylglyoxime in Ammonia and Alcohol Solutions with the Aid of Amperometric Titration," Zhur. Analit. Khim., 4, No. 5, 1949.

Manufactors Analysis, quantitative duality Analysis, quantitative duality Analysis, quantitative duality of Dimethylglyoxime in the Ada of the Solubility of Dimethylglyoxime in Amonola and Alcohol Solutions With the Ada of Calyanskay, Inst of Chem and Metal, Ural Affilliate, Acad Sci USER, 5½ pp "Zhuranskay, Inst of Chem and Metal, Ural Affilliate, Acad Sci USER, 5½ pp "Zhur Anal Khim" Vol. IV, No. 5, c., 286-29/ In the instance of dimethylglyoxime, expediency of using amperometric titration for determining solubilities of slightly soluble organic compounds is shown. Solubility of this compound in agreeous is shown. Solubility of this compound in agreeous is shown. Solubility of this compound in agreeous in the namonia concentration interval of 0.01-10 M, and 1.0-10.0 M, (2) ammonium ton-amonia and an ammonium chloride concentration interval of 0.01-1.0 M, and (3) alcohol solutions with an alcohol solution wi	0
AELYANSKAYA, A.I. A. S.	



SOV/137-59-1-2171

V. P.

Translation from: Referativnyy zhurnal. Metallurgiya, 1959, Nr 1, p 285 (USSR)

Zelyanskaya, A. I., Bykov, I. Ye., Gorshkova, L. S. AUTHORS:

On the Separation of Selenium and Tellurium by a Cationite TITLE:

(K voprosu o razdelenii selena i tellura kationitom)

PERIODICAL: Tr. In-ta metallurgii; Ural'skiy fil. AN SSSR, 1957, Nr 1, pp 151-154

ABSTRACT: For a quantitative separation of Se from Te, as well as from Ce, Fe and Zn, pH 1.4 solutions are passed through the "espatig" [transliterated KU-1 cationite. Te, Cu, Fe, Pb, and Zn are completely absorbed by the cationite. Te is then extracted with a solution of NH4OH (1:2), and the cationite is washed with H2O and 5% HCl to a neutral reaction. It is shown that Se can be quantitatively separated from Cu, Fe, and Zn. The presence of Pb lowers the results. Hydrochloric acid solutions and ammoniacal solution containing sodium versenate are suitable for separating Se and Te from Cu, Fe,

and Zn. Se passes through into the filtrate in all cases.

Card 1/1

CIA-RDP86-00513R001964410016-9" APPROVED FOR RELEASE: 07/19/2001

ZELYANSKAYA, A.I.; BYKOV, I.Ye.; GORSHKOVA, L.S.

Polarographic determination of tetravalent selenium and tellurium when both are present. Trudy Inst. met. UFAN SSSR no.1:155-160 157. (MIRA 11:9)

(Selenium) (Tellurium) (Polarography)

CIA-RDP86-00513R001964410016-9" APPROVED FOR RELEASE: 07/19/2001

SOV/137-58-11-23831

Translation from: Referativnyy zhurnal. Metallurgiya, 1958, Nr 11, p 280 (USSR)

AUTHORS: Zelyanskaya, A. I., Bykov, I. Ye., Gorshkova, L. S.

TITLE: Effect of Heavy Metals on the Polarographic Waves of Selenium and

Tellurium (Vliyaniye tyazhelykh metallov na polyarograficheskiye

volny selena i tellura

PERIODICAL: Tr. In-ta metallurgii. Ural'skiy fil. AN SSSR, 1957, Nr 1, pp 161-

169

ABSTRACT: The authors investigate the effect of some heavy metals on the po-

larographic waves of Se and Te in the NH₃NH₄Cl solution. The Cu wave precedes the Te wave, and two separate waves appear on the polarogram, but when the ratio Cu:Te>l the Te wave is appreciably lowered and a preliminary separation of Cu is necessary. Zn, which is reduced at a more negative potential, does not affect the Te wave; however, at a Te:Zn>l ratio Te lowers the Zn wave. Pb adsorbs Te when it precipitates; when Na versenate B is added, Pb is reduced

at a more negative potential than Te, whereas the addition of gelatine displaces the $E_{1/2}$ of Pb to -1.3 v. The presence of 0.05% gelatine

Card 1/2 completely suppresses the Pb wave, after which the determination

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SOV/137-58-11-23831

Effect of Heavy Metals on the Polarographic Waves of Selenium and Tellurium

of Te proceeds without impediments. The impeding effect of Fe is eliminated by the addition of 0.1 mole/liter of tartaric acid and 0.1% gelatin; in this case Fe is reduced at a more negative potential than Te and has no effect on the magnitude of its wave. Determination of Se is impeded by the presence of Cu, Pb, Cd, and Fe. When the molar concentration ratio Te:Se > 1 Te also impedes the determination. The effect of Zn, Ni, and Co²⁺ is eliminated by the addition of Na versenate B.

N.B.

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Zelvanskava, A.I.:	Bykov, I.Ye.; and Gorshkova, I	of Heavy 555 rudy, vyp 1,)(AS USSR, Ural L.S. The Separation of	Affil,)
Selenium and Tellu	rium by a Cationite		151
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Zelyanskaya, E. 庭.

B-12

USSR/Physical Chemistry - Electrochemistry.

Abs Jour: Referat. Zhurnal Khimiya, No 2, 1958, 3980.

Author : I.Ye. Bykov, A.I. Zelyanskaya. Title : Influence of Tellurium on Polarographic Wave of Selenium. Inst : Academy of Sciences of USSR.

Orig Pub: Izv. vost. fil. AN SSSR, 1957, No 2, 47-51.

Abstract: The presence of SeO₃² does not influence the height of the TeO₃² wave on the background of 0.5 M NH₄Cl + 0.5 M NH₄OH. The height 2 wave of the SeO₃² wave does not change up to Te: Se = 1. The SeO₃² wave becomes lower at a higher relative content of TeO₃². In wave becomes lower at a higher relative content of TeO₃² reduction the author's opinion, Se² ions forming at the SeO₃² as follows: the author's opinion, Se² ions forming at the SeO₃² as follows: diffuse into the solution and react with TeO₃² as follows: 2Se² + TeO₃² + TeO₃² + 6H⁴ - 2Se + Te + 3H₂O. In order to verify this assumption, a SeO₃² solution was electrolyzed on a carbon cathode, after which an anode-cathode wave was revealed on the

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, No 2, 1958, 3980.

of this solution to another remained unchange RDP86-00513R001964410016-Te032- wave differenced in the case of sec. and reo32- and reo32- and reo32- and reo32- but the sec also RZhKhim, 1955, 29202.

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137-58-4-8652

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 4, p 333 (USSR)

AUTHORS: Zelyanskaya, A.I., Bausova, N.V.

TITLE:

Separation of Gallium from Zinc, Copper, Cobalt, Nickel, and Iron by Ion Exchange (Otdeleniye galliya ot tsinka, medi, kobal'ta, nikelya, i zheleza metodom ionnogo obmena)

PERIODICAL: Izv. vost. fil. AN SSSR, 1957, Nr 7, pp 51-53

ABSTRACT:

Polarographic determination of Ga in a passive electrolyte of the following composition: 0.1 M Na salicylate, 0.1 M NaCl, pH 2.5-3.8 is inhibited by Co, Ni, Zn, and large amounts of Cu. SBS cationite was used in the Na form in columns of 1 cm diameter, 50 cm high, to remove the inhibiting impurities. The resin, of 0.25-0.5 mm grain size, was charged to a height of 25 cm. A 100-cc solution containing 15 cc concentrated NH4OH and 10 cc 2N. NaOH was transmitted through the resin at a rate of 5 cc/min, as a result of which the Ga remained in the filtrate in its entirety, and the Ni, Co, Zn, and Cu underwent quantitative absorption by the cationite. The resin was washed by a 100-cc solution containing 10 cc concentrated NH4OH and 5 cc 2N. NaOH. The filtrate and the wash waters were evaporated down to a

Card 1/2

137-58-4-8652

Separation of Gallium (cont.)

volume of 25 cc and were neutralized by 6N HCl (methylorange test), and the Ga was determined polarographically. Extraction of the Ga in the filtrate attained 98-100% when the solution contained 0.5-5.0 mg.

1. Gallium--Determination 2. Gallium--Separation. 3. Gallium--Polarographic analysis 4. Ion exchange resins--Applications

Card 2/2

sov/137-58-11-23830

Translation from: Referativnyy zhurnal. Metallurgiya, 1958, Nr 11, p 280 (USSR)

AUTHORS: Zelyanskaya, A. I., Bykov, I. Ye., Gorshkova, L. S.

TITLE:

Polarographic Determination of Quadrivalent Selenium and Tellurium When Both are Present (Polyarograficheskoye opredeleniye chetyrekh-walentnykh selena i tellura pri sovmestnom ikh prisutstvii)

PERIODICAL: Tr. In-ta metallurgii. Ural'skiy fil. AN SSSR, 1958, Nr 1, pp 155-

ABSTRACT:

It is established that for the joint polarographic determination of Se and Te a basic electrolyte containing (in mole/liter) (NH₄Cl 0.75, NH₄OH 0.25, Na₂SO₃ 0.1 is the most suitable. In order to eliminate the maxima, the polarographic analysis is performed in the presence of 0.002% gelatine: E_{1/2} of Te = -0.9 v and E_{1/2} of Se = -1.5 v (sateurated control electrolyte). An increase in the concentration of gelatine causes a displacement of the Se wave in the negative sense, and its determination becomes impossible. Se can be determined polarographically at concentrations of 0.05-2 numble diterate molaroconcengraphically at concentrations of 0.05-2 numble diterate molaroconcentration of Te should not be higher than the Se concentration lest the Se wave be lowered. Nitrates and heavy metals should be absent. To

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SOV/137-58-11-23830

Polarigraphic Determination of Quadrivalent Selenium and Tellurium (cont.)

dissolve Se and Te the precipitate of elemental Se and Te is obtained by any method and to this, together with the filtrate, 5 cc of freshly prepared solution of 25 mg KClO3 in HCl (1:1) are added. The mixture is stirred, heated slightly, and upon dissolution neutralized with NH4OH to methyl orange. The solution together with the paper, is transferred into a 50-cc flask, basic electrolyte is added to the mark, and the mixture is analyzed polarographically. The method was verified on specimens of dust and cake. Two-gram samples were used for the analysis.

N. G.

Card 2/2

SOV/137-59-2-4765

Translation from: Referativnyy zhurnal. Metallurgiya, 1959, Nr 2, p 343 (USSR)

AUTHORS: Zelyanskaya, A. I., Bausova, N. V., Kukalo, L. Ya.

TITLE: Study of Polarographic Properties of Gallium and Indium (Izucheniye

polyarograficheskikh svoystv galliya i indiya)

PERIODICAL: Tr. In-ta metallurgii. Ural'skiy fil. AN SSSR, 1958, Nr 2, pp 263-

ABSTRACT: Investigations were carried out for establishing the optimum conditions for polarographic determination of Ga and In. It was established that in acid salicylate solutions (0.1 M Na salicylate and 0.1 M NaCl with a pH of 2.5 - 3.8) Ga forms a well defined wave with E_{1/2} = -0.99 v (in saturated standard electrolyte); introduction of gelatin has a negative effect. The electrode reaction corresponds to a three-electron reduction and proceeds irreversibly. With an increase of the salicylate content in the solution E_{1/2} shifts in the negative sense. The polarographic determination is not impeded by Al, As⁵⁺, Mn⁷⁺, and small amounts of Cu, Bi, Sb, Fe, In, Cd, Pb, and Tl. Zn, Ni, Co, Mo, and Sn should be first removed. In is read polarographically

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against the background of 3N HCl in the presence of 0.01% solution

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Study of Polarographic Properties of Gallium and Indium

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of gelatin; $E_{1/2}$ =-0.78 v. An increase in gelatin concentration decreases sharply the intensity of the diffusion current.

N. G.

Card 2/2

SOV/137-59-2-4837

Translation from: Referativnyy zhurnal. Metallurgiya, 1959, Nr 2, p 353 (USSR)

AUTHORS: Bykov, I. Ye., Zelyanskaya, A. I., Gorshkova, L. S.

TITLE: Polarographic Determination of Tetravalent Selenium and Tellurium

(Polyarografiya chetyrekhvalentnykh selena i tellura)

PERIODICAL: Tr. In-ta metallurgii. Ural'skiy fil. AN SSSR, 1958, Nr 2, pp 275-

279

ABSTRACT: The authors examined the parameters of the polarographic determina-

tion of Se and Te. In acid solutions their reduction proceeds with formation of several waves, whereas in strong alkaline solutions the Se-wave disappears. Polarographic determination of Se and Te when both are present is carried out in an electrolyte of the following composition (in mole/liter): NH₄Cl 0.5, NH₄OH 0.5, Na₂SO₃ 0.1, gelatin 0.002°/o, at a pH ~9. With a concentration of gelatin > 0.01°/o the Se wave blends with the terminal ascending branch of the polarogram. In the presence of a number of heavy metals a decrease of the diffusion current of Se

and Te is observed; moreover, the Se wave decreases in the presence of Te. However, in small amounts of the elements the dependence of

Card 1/2 the Se wave on Te is imperceptible. The authors developed a technique

SOV/137-59-2-4837

Polarographic Determination of Tetravalent Selenium and Tellurium

for determination of Te in the presence of Fe (in a tartaric-acid solution), or Te in the presence of Pb, of Se in the presence of Zn (in an E.D.T.A. solution), and of Te in the presence of Gu (alcaline cyanide solution). In order to determine Se and Te in products of complex composition it is necessary to separate them from other elements first.

N. G.

Card 2/2

SOV/137-58-11-23803

Translation from: Referativnyy zhurnal. Metallurgiya, 1958, Nr 11, p 275 (USSR)

AUTHORS: Zelyanskaya, A. I., Bausova, N. V.

Polarographic Investigation of the Gallium Salicylate Complex (Polyarograficheskoye issledovaniye salitsilatnogo kompleksa

galliya)

PERIODICAL: Izv. Sibirsk. otd. AN SSSR, 1958, Nr 3, pp 52-59

ABSTRACT: The authors established the feasibility of the polarographic determ-

ination of Ga against a background of 0.1M solution of Na salicylate and 0.1M solution of NaCl at a pH of 2.5-3.8; the addition of gelatin produces a negative effect. The stability of the Ga salicylate complex is comparatively low because the constant of instability K = 1.93.10.6. The potential of the half wave of Ga = -0.988 v (saturated electrolyte). The electrode reaction is irreversible and corresponds to a 3-electron reduction. W, Al, Mn⁷⁺, As⁵⁺, alkaline, and alkaline-earth metals do not impede the reaction; neither does Fe at a ratio Ga:Fe <1:35. Cu, In, Tl, Cd, Pb, and Sn are reduced at more positive potentials and in small amounts have no effect. Mn²⁺ is reduced close to Ga, therefore it should be oxidized to Mn⁷⁺. Under these conditions Bi

Card 1/2

TITLE:

SOV/137-58-11-23803

Polarographic Investigation of the Gallium Salicylate Complex (cont.)

is hydrolyzed; however, when its content is \$10 mg, no adsorption of Ga is observed. Sn is hydrolyzed causing an adsorption of Ga; therefore, its preliminary removal is necessary. The presence of Mo impairs the polarographic wave of Ga. Zn, Ni, and Co impede the determination of Ga owing to the proximity of their reduction potentials.

Card 2/2

STASHKOVA, N.V.; ZELYANSKAYA, A.I.

Polarographic determination of germanium. izv.Sib.ots. AN SSSR no.1:59-66 '59. (MIRA' 12:4)

1. Ural'skiy filial AN SSSR. (Polarography)

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ZELYANSKAYA, A.I., GORSHKOVA, L.S.

Determination of small amounts of selenium in anode copper-Trudy Inst.met.UFAN SSSR no.5:137-139 *60. (MIRA 13:8) (Copper--Analysis) (Selenium--Analysis)

ZELYANSKAYA, A.I.; GORSHKOVA, L.S.

Polarographic method of determining tellurium in copperbearing and leaded compounds. Trudy Inst.met.UFAN SSSR no.5:141-144 '60. (MIRA 13:8) (Polarography) (Tellurium)

Mechanism of the reduction of tetravalent germanium on dropping mercury electrodes. Izv. Eib. otd. AN SSSR no.1:72-81 '61.

(MIRA 14:2)

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ZELYANSKAYA, A.I.; KUKALO, L.Ye.

Polarographic reduction of gallium in a pyrocatechol solution. Zhur.anal.khim. 18 no.6:726-728 Je '63. (MIRA 16:9)

1. Institute of Metallurgy, Ural Branch of the Academy of Sciences of the U.S.S.R., Sverdlovsk.

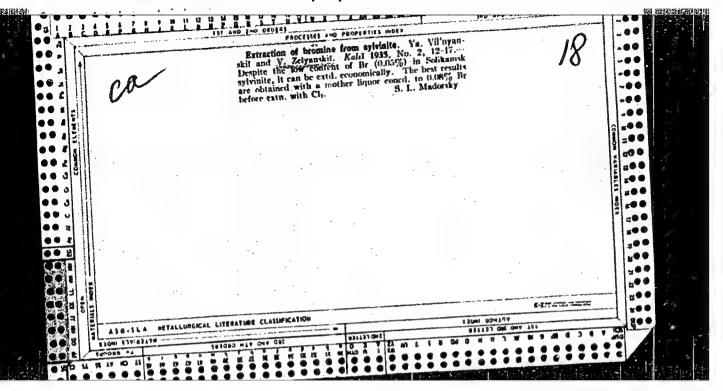
(Gallium compounds) (Polarography) (Pyrocatechol)

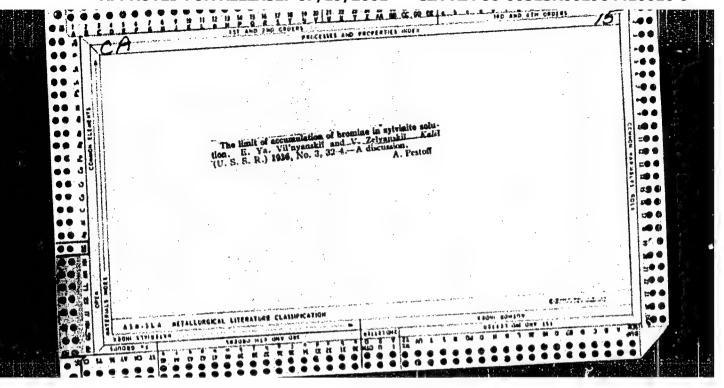
ZELYANSKAYA, A.I.; STASHKOVA, N.V.

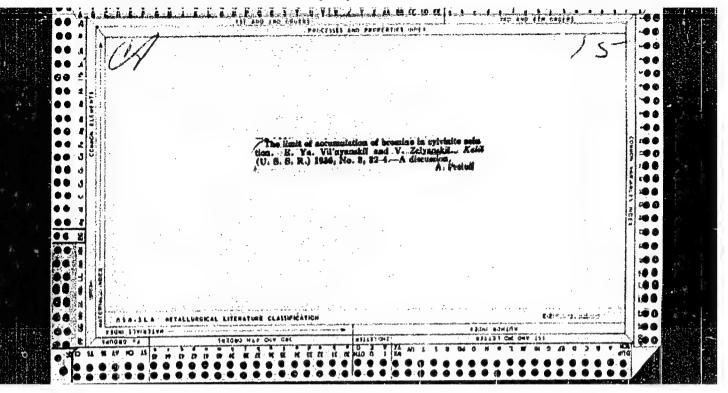
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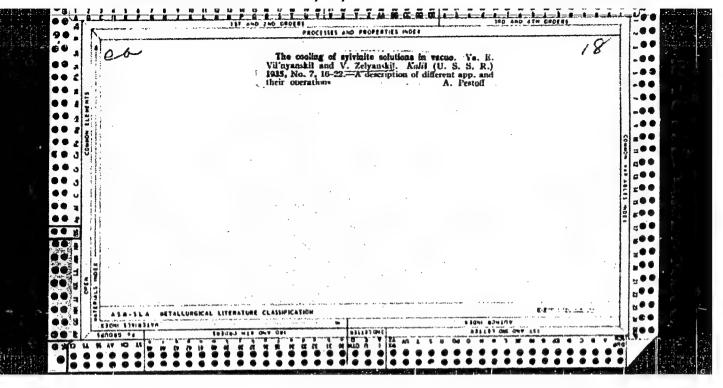
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MEL'NIKOV, Nikolay Prokof'yevich, doktor tekhn. nauk, prof.; ZELYATROV, V.N., inzh., nauchn. red.

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MILLER, Viktor Yakovlevich, inzh.; KORCHAGIN, Vladimir Aleksandrovich, inzh.; TOLOKONNIKOV, Vladimir Gerasimovich, inzh., MUKHANOV, K.K., kand. tekhn. nauk, retsenzert; KUZNETSOV, V.V., inzh., retsenzent; ZELYATROV, V.N., inzh., nauchn. red.

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[Selection of steel for metal construction elements; a manual for designers] Vybor stali dlia stroitel'nykh metallicheskikh konstruktsii; posobie dlia proektirovshchikov. Moskva, Stroiizdat, 1964. 97 p. (MIRA 17:3)

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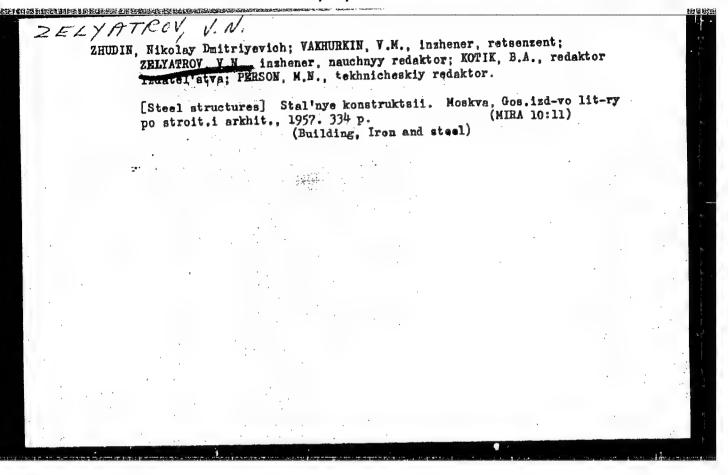
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ZELYATROV. V.N., nauchnyy redaktor; YEGOROVA, N.O., redaktor isdatel stva;

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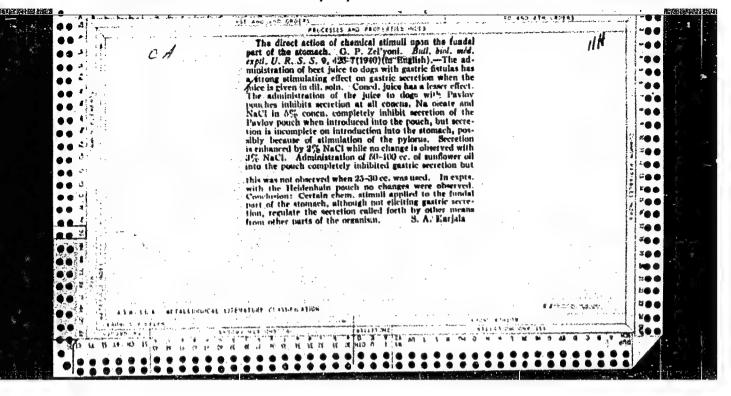
(Steel, Structural)

LESSIG, Yevgeniy Nikolayevich; LILETEV, Aleksandr Fedorovich; SOKOLOV, Aleksandr Georgiyevich; ZELYATROV, V.H., nauchnyy redaktor; ROSTOVISEVA, M.P., redaktor izdatel stva; TOKKE, A.H., tekhnicheskiy redaktor

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ZELYAYEV, A.F.: SHUNOV, K.M.; ALEKSEYEV, Yo.N.

Diaphragm tensometric manometer. Zav.lab.22 no.11:1368-1369 '56. (Manometer) (MLRA 10:2)



ZELYAYEV, A.F.

USSR/Processes and Equipment for Chemical Industries - K-2

Control and Measuring Devices. Automatic Regulation.

Abs Jour : Referat Zhur - Khimiya, No 9, 1957, 33322

Author : Zelyayev, A.F., Shumov, K.M., Alekseyev, Ye.N.

Inst : Title : Tensimetric Diaphragm Manometer

Orig Pub : Zavod. laboratoriya, 1956, 22, No 11, 1368-1369

Abstract : In the tensimetric diaphragm manometer developed by the au-

thors the pressure that is being determined distorts a circular steel diaphragm and a wire-resistor primary element fastened thereon. Change in ohmic resistance of the primary element is measured by means of a 4-branch bridge. The manometer consists of a cylindrical housing into which is threaded a cover with an aperture which provides an outlet to the atmosphere. The diaphragm with the primary element fastened thereto is clamped between housing and cover.

On a plate that is located on the cover is fastened a

Card 1/2

USSR/Processes and Equipment for Chemical Industries - K-2 Control and Measuring Devices. Automatic Regulation.

Abs Jour : Ref Zhur - Khimiya, No 9, 1957, 33322

primary element which compensates the temperature distortion of the primary element of the diaphragm. Pressure from the system under study is admitted into a bottom chamber through a connection tube. The apparatus is suitable for measuring static and dynamic pressure and vacuum. With a relative distortion of the diaphragm not exceeding 0.2-025% the apparatus has a rectilinear response. In the experimental studies diaphragms 50 mm in diameter were used. Use of a diaphragm of larger diameter is disadvantageous since on increase of the diameter the frequency of the natural oscillations of diaphragms decreases. Diaphragms having a thickness from 0.1 to 7 mm were used to measure pressures from 0.004 to 900 kg/cm², respectively.

Card 2/2

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I 19739-63 EWP(r)/EDS AFFTC/APGC EM
ACCESSION NR: AT3002160 S/2919/62/000/000/0112/0151

AUTHOR: Zelyukova, R. V.

TITLE: Vibration damping in link rods

SOURCE: Voprosy rasseyaniya energii pri kolebaniyakh uprugikh sistem; trudy nauchno-tekhnicheskogo soveshchaniya. Kiev, Gostekhizdat USSR, 1962, 112-151

TOPIC TAGS: vibration damping, link rod, logarithmic decrement, forced vibration

ABSTRACT: Experimental and analytical investigations were made to determine the damping capacities of two types of link rods, one having a clearance in the joint and the other with a metallized cover. Experiments were carried out on an apparatus of IsNIITMASh (Central Scientific Research Institute of Technology and Mechanical Engineering) specification. The damping characteristics were obtained on the assumption of a two-term, linear logarithmic decrement, thus

 $\delta(\xi_0) = \delta_0 + k\xi_0 \tag{1}$

where δ_0 , k - deforming capacity of rod in low and high deformation regions (0.1 kg/mm² and 10 kg/mm² or over) respectively; and ξ_0 - integrated magnitude depending on type and intensity of stress and type of rod under study. Some basic results Card 1/2

L 19739-63 ACCESSION NR: AT3002160 and conclusions drawn from the experiment are: the metallized cover type rod follows a linear damping law given by equation (1) above in the stress range 50-600 and 100-800 kg/cm2 with a cover deposit of high carbon steel 1-2.5 mm thick. The parameter of increases by a factor of 2-5.8 and k increases by 7-11. Furthermore, both types of rods are found to be applicable in carrying vibrational loads under practical operating conditions. On the basis of the assumption that the hysteresis loop of the link rod with an external harmonic forcing function is elliptic in form equations are derived for rod displacements both in free and forced vibrations. It is shown that the coupling between a large damping factor and the resonance amplitude induce an inherent stability in the vibrating system. Orig. art. has: 14 equations, 4 figures, and 1 table. ASSOCIATION: none SUBMITTED: 00 00 DATE ACQ: 10May63 ENCL: SUB CODE: NO REF SOV: OTHER: 001

